

# Numerical approaches to evaluate the hydraulics of Vertical Slot Fishways

### A comparative study of 2D and 3D simulations

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European Union Horizon 2020 Research and Innovation Programme: Marie Sklodowska-Curie Actions, Grant Agreement No. 860800







River connectivity has been affected by human development

Grill et al. (2019)

VSFs are the most common and most studied fishways worldwide

Fuentes-Pérez et al. (2017)

**AD Ribes** 

VSF design efficiency are still a challenge (54% - 63%).

Bunt et al. (20012

90% efficiency is required to achieve restoration of connectivity

Lucas & Baras (2001)

CFD methodologies have already been applied for evaluating VSFs

Powerful open-source tools are available, OpenFOAM & TELEMAC2D





## **Vertical Slot Fishways**

#### **Design requirements**

- A VSF should provide suitable migration pathway and resting zone
- Baffles provide a vertical passing slot
- Jets should be clearly defined for upstream guidance
- Recirculation zones should be large enough to provide suitable resting zones
- Volumetric power dissipation should be in the range 150 – 200 W/m<sup>3</sup>
- VSF dimensions are related to the biological requirements of the targeted species.







## Vertical Slot Fishways

#### **Hypothesis**

 Fully 3D hydraulic behavior is rarely found in the working discharges on VSF. Therefore, hydraulics can be represented by both 2D and 3D simulations

#### **Objectives**

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- To evaluate the hydraulics of VSF through numerical simulations applying open-source modelling tools
- To explore the advantages and disadvantages of 2D and 3D modelling approaches
- To evaluate the influence of physical parameters (slope, friction)







#### Mild – slope

Bombač et. al (2015).

Built at Arto-Blanca hydropower plant in Slovenia

RIBES

Scale model 1:1

2D & 3D simulations

ADV measurements from 4 cross sections

#### Geometry

L<sub>p</sub>: 3.0 m

B : 2.2 m

N:5 pools

Slope : 0.0167 m/m









#### Steep - slope

Chorda et. al (2010).

Laboratoire d'Etudes Aérodynamicques, France

Scale model 1:4

**2D** simulations

RIBES

ADV and PIV measurements from 2 cross sections

#### Geometry

- L<sub>p</sub>: 3.0 m
- B : 2.0 m
- N:5 pools
- Slope : 0.1 m/m

5





### Theoretical Background:

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#### **Three – dimensional simulations**



## Theoretical Background:

#### **Two – dimensional simulations**



$$\frac{\partial h}{\partial t} + \frac{\partial (h u_i)}{\partial x_i} = 0; \qquad i, j = 1, 2$$

$$\frac{\partial u_i}{\partial t} + u_j \frac{\partial u_i}{\partial x_j} = -\frac{\partial Z}{\partial x_i} + S_f + \frac{1}{h} \frac{\partial}{\partial x_j} \left( h v_t \left( \frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right) \right)$$
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Mild - slope, S = 1.67%, Q = 1.0 m<sup>3</sup>/s



Steep - slope, S = 10.0%, Q = 0.735 m<sup>3</sup>/s







Velocities and turbulent kinetic energy are well represented in every cross sections (XS).

- Turbulent kinetic energy is better reproduced in 3D simulations
- Coarser 3D simulations tend to overestimate the velocities
- *y*-velocities are close to zero. Therefore, relative error is sensitive to small changes



### Validation: Mild slope



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### **Results: Steep slope**



In the cross section, closer to the slot, 2D simulations tend to overestimate turbulent kinetic energy.

- 3D simulations tend to overestimate the velocities.
- Mesh size does not improve the representation velocity representation closer to the slots
- Turbulent kinetic energy is better represented in the middle of the pool



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### Ribes Results: Impact of friction coefficient



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RIBES 2D Simulation

- 1.4

- 1.2

- 1.0

0.8 (m/s)

0.6

0.4

0.2

0.0

- 1.4

1.2

- 1.0

0.8 [*m*] 0.8

0.6

0.4

0.2

0.0

15.5

**3D Simulation** 

15.5

2 W-=0.1 6.2 0.4 0.5 0.8 ۶ [m] 1.0 1.25 1.295 0 0 2 3 x [m]

Bombač, M., Novak, G., Mlačnik, J. & Četina, M. (2015). Extensive field measurements of flow in vertical slot fishway as data for validation of numerical simulations. EcologicalEngineering, 84, 476–484. https://doi.org/10.1016/j.ecoleng.2015.09.030



2.00

1.75 1.50

1.25

1.00

0.75

0.50

0.25

0.00 12.5

2.00

1.75 1.50

1.25

1.00

0.75

0.50

0.25 0.00

12.5

13.0

13.0

13.5

13.5

14.0

14.0

14.5

14.5

15.0

15.0



## Model Comparison

#### **3D Simulations (OpenFOAM)**

Simulations met the validation criteria for velocities and turbulent kinetic energy

Mild & Steep slope hydraulics was successfully reproduced

Flow patterns outcome reproduced flow topology observed experimentally

It is computationally demanding

#### **2D Simulations (TELEMAC-2D)**

Simulations met the validation criteria for velocities.

Turbulent kinetic energy was not reproduced in the steep – slope VSF

Flow patterns missed some recirculation zones measured experimentally

Model setup and computing is much faster than 3D simulations





## Conclusions and recommendations

- For all cases considered in this study, the simulation results met the validation criteria. However, accuracy was different from one case to another.
- Two dimensional simulations displayed a considerable overestimation of turbulent kinetic energy, especially in the steepest case close to the slots.
- Variation in the friction coefficient did not significantly affect the accuracy of the 2D simulations.
- When the computational resources are available, 3D simulations should be preferred over 2D simulations.









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# Thank you!

Questions...



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**Ribes**